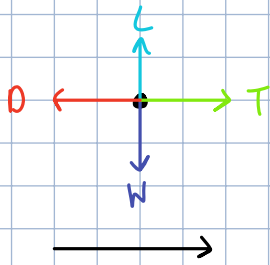


Treating an aircraft as a point mass :



for an aircraft in equilibrium

$$L = W$$

$$\rightarrow C_L = \frac{L}{\frac{1}{2}\rho V^2 S} = \frac{W}{\frac{1}{2}\rho V^2 S} = \frac{w}{q}$$

wing loading $\frac{W}{S}$
dynamic pressure $\frac{1}{2}\rho V^2$

The corresponding flight speed is therefore :

$$V = \sqrt{\frac{w}{\frac{1}{2}\rho C_L}}$$

$\therefore \downarrow V$ from $\downarrow w$ (lighter / bigger wing)
 $\uparrow C_L$ ($\uparrow a$)
 $\uparrow \rho$

Minimum possible level flight speed occurs at $C_{L_{max}}$ (stall)

Equivalent Air Speed :

True air speed (TAS) V or V_T is speed relative to air mass in which it's flying

Equivalent air speed is the speed at standard sea level density that gives the same aerodynamic loads.

$$V_E = \sqrt{\frac{\rho}{\rho_0}} V = V \sqrt{\sigma}$$

EAS is close to indicated air speed (IAS), measured via a pitot-static tube to measure q .

$$p_{\text{pitot}} - p_{\text{static}} = \frac{1}{2}\rho V^2 = \frac{1}{2}\rho_0 V_E^2 \quad \text{Bernoulli}$$

Stall will always occur at same EAS and structural limits defined in terms of EAS.

Drag :

$$D = T \text{ in eqm} \quad \therefore \quad C_D = \frac{T}{\frac{1}{2} \rho V^2 S}$$

There are many additional sources of drag :

- Profile (skin + form)
- Interference : between components

.....

Drag Equation

- Drag consists of zero-incidence coefficient C_{D_0}

- part $\propto C_L^2$

↳ induced drag + form drag \rightarrow drag due to lift

$$C_D = C_{D_0} + K C_L^2$$

$$K = \frac{1}{\pi e AR}$$

Also written as

$$C_D = C_{D_0} + \frac{C_L^2}{\pi e AR}$$

where e is redefined from span efficiency factor for wing to Oswald efficiency factor for the whole aircraft.

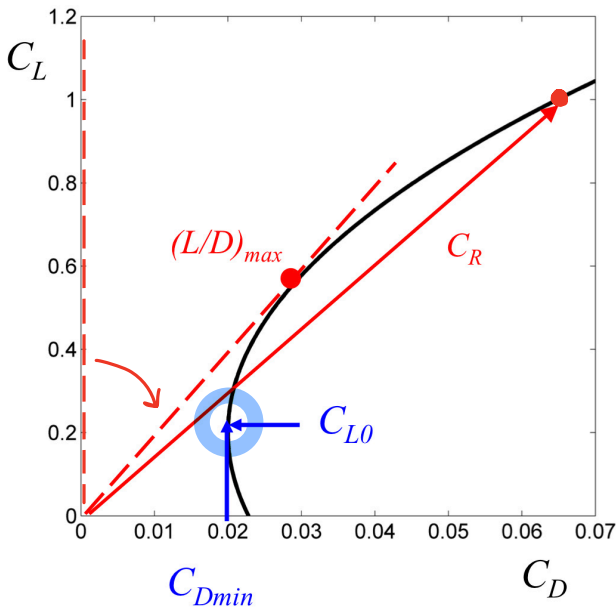
Drag Polar :

- For an aircraft with a cambered wing, minimum drag no longer necessarily occurs at 0 lift

↳ (we will assume $C_{D_{min}} = C_{D_0}$ for year 1)

\rightarrow drag equation becomes $C_D = C_{D_{min}} + K (C_L - C_{L_0})^2$

Sometimes plotted as C_L vs. C_D



L/D_{max} is tangent passing through origin

A line from origin to any point on graph is the vector of the aero force at that point. (C_R)

Drag Equation Expanded :

$$C_D = C_{D0} + KC_L^2 \quad \longrightarrow \quad C_D = C_{D0} + \frac{KW^2}{\left(\frac{1}{2}\rho V^2 S\right)^2}$$

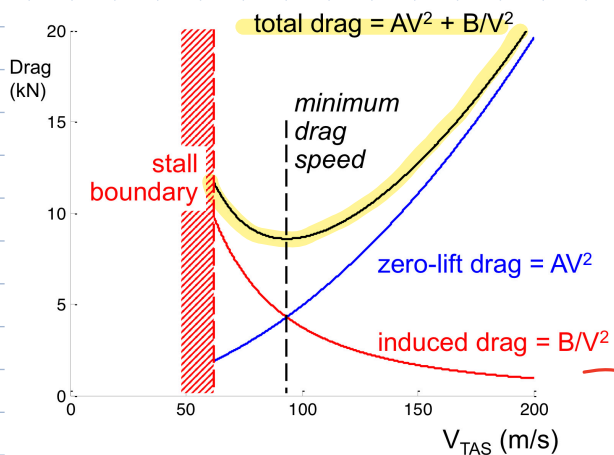
$$C_L = \frac{W}{\frac{1}{2}\rho V^2 S}$$

$$D = C_{D0} \frac{1}{2}\rho V^2 S + \frac{KW^2}{\frac{1}{2}\rho V^2 S}$$

$$D = AV^2 + \frac{B}{V^2}$$

where A is 0 lift drag term, $A = C_{D0} \frac{1}{2}\rho S$
 and B is induced drag term, $B = \frac{KW^2}{\frac{1}{2}\rho S}$ } functions of alt. & ρ

Drag as function of velocity : (at SL)

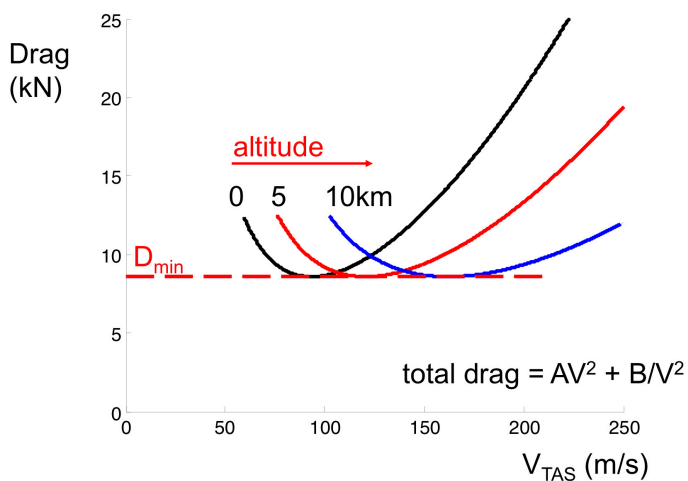


\uparrow as $V \uparrow$: at high speed term A dominates

\downarrow as $V \uparrow$: at low speed B dominates

Drag changing w/r to altitude :

Drag at Altitude



As altitude \uparrow , $\rho \downarrow$ and therefore we must fly faster ($V \uparrow$) to achieve steady level flight.

Alt. \uparrow , $\rho \downarrow$, $V \uparrow$

D_{min} doesn't change as V & ρ both affect drag and balance with changing altitude.

if plotted in terms of EAS, variation with altitude disappears

Drag equation in terms of EAS :

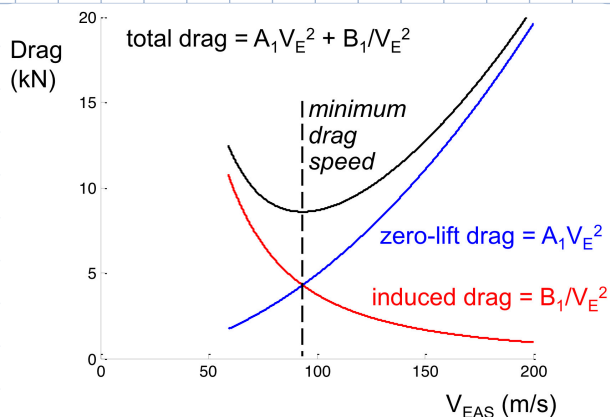
$$D = A_1 V_E^2 + \frac{B_1}{V_E^2}$$

where $A_1 = C_{D0} \frac{1}{2} \rho_0 S$

and $B_1 = \frac{KW^2}{\frac{1}{2} \rho_0 S}$

constants as ρ constant (ρ_{SL})

one curve describes aircraft drag vs. V rather than many with changing alt.



Minimum Drag :

$$D = L \times \left(\frac{D}{L}\right) = W \times \left(\frac{C_D}{C_L}\right)$$

\therefore min drag at min $\frac{C_D}{C_L}$

$$\frac{C_D}{C_L} = \frac{C_{D0} + KC_L^2}{C_L} = \frac{C_{D0}}{C_L} + KC_L$$

$$\frac{d(C_D/C_L)}{dC_L} = -\frac{C_{D0}}{C_L^2} + k$$

at min where = 0

$$C_{D0} = KC_L^2$$

∴

$$C_{Dmin} = 2C_{D0} = 2KC_L^2$$

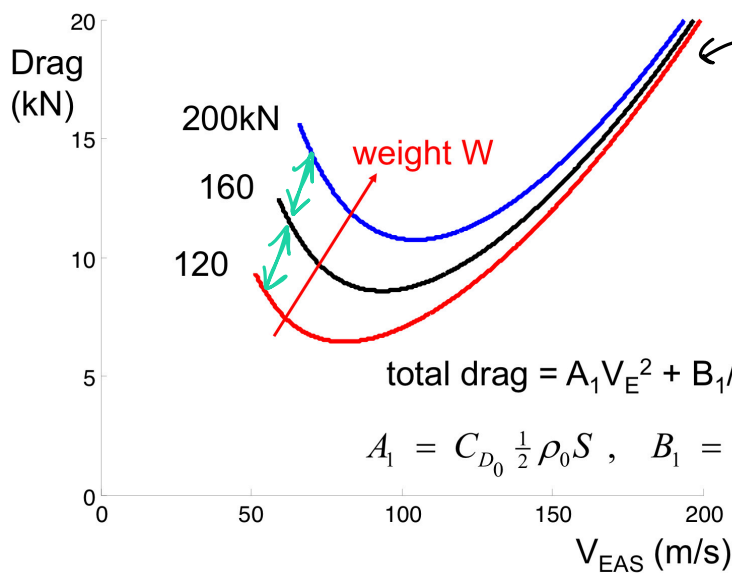
$$\left(\frac{C_D}{C_L}\right)_{min} = 2\sqrt{C_{D0}K}$$

$$C_{LMO} = \sqrt{\frac{C_{D0}}{K}}$$

Subbing into V equation, $V = \sqrt{\frac{W}{\frac{1}{2}\rho S C_L}}$

$$\rightarrow V_{MO} = \left(\frac{2W}{\rho S}\right)^{\frac{1}{2}} \left(\frac{K}{C_{D0}}\right)^{\frac{1}{4}}$$

Effect of Weight on Drag:



at $\uparrow V$ induced drag B becomes less significant
B includes W term
so disparity at $\uparrow V$ becomes small

whereas at low speed B dominates
→ large difference